## In the Claims:

This listing of claims will replace all prior versions, and listings, of claims in the application.

- 1. (Currently amended) Method to supply a defined fluid flow, especially for liquid chromatography,
  - a) in which a total flow  $(f_0)$  is split into an internal excess flow  $(f_{ie})$  in an excess branch and an internal work flow  $(f_{iw})$  in a working branch,
  - b) wherein the split ratio between the internal work flow  $(f_{iw})$  and the internal excess flow  $(f_{ie})$  is determined by the reverse ratio of a fluidic resistor (7) in the working branch and fluidic resistor (9) in the excess branch, and
  - c) where the excess branch and the working branch are interconnected at the outputs of the two fluidic resistors (7, 9) via a cross-branch,
  - d) in which the balance flow  $(f_{bal})$  [[occurring]] occurring between the outputs of the fluidic resistors (7, 9) is measured with a flow sensor (108),
  - e) where further down the working branch an external work flow (f<sub>ew</sub>) can be supplied to an operating device downstream of the device (100), [[a chromatography column, for example, ]]
  - f) after which further down the excess branch an [[adjustabe]] adjustable resistance device (11) is installed,
  - where by control of the resistance value of the adjustable fluidic resistance device (110) the balance flow  $(f_{bal})$  is regulated in such manner that the balance flow  $(f_{bal})$  [[preferably]] is in the temporal median, generally equal to zero or equal to a preset offset value, whose value is small in comparison to the internal work flow  $(f_{iw})$ .
- 2. (Original) Method according to claim 1, wherein the preset offset value for the balance flow  $(f_{bal})$  is greater than zero, whereby the positive sign indicates a flow from the working path in the direction of the excess path.

- 3. (Currently amended) Method according to claim 1, [[or 2,]] wherein the dependency of the sensor signal (S<sub>bal</sub>) of the flow sensor (108) on at least one property of the fluid [[, especially the thermal conductivity or thermal capacity of the fluid,]] is corrected in such fashion during the adjustment of the balance flow (f<sub>bal</sub>) that the preset offset value for the balance flow (f<sub>bal</sub>) results.
- 4. (Currently amended) Method according to claim 3, wherein for the correcting purposes a correction parameter is linked to the sensor signal (S<sub>bal</sub>). [[, in particular a correction factor is multiplied with the sensor signal (S<sub>bal</sub>).]]
- 5. (Currently amended) Method according to claim 3, [[or 4,]] wherein the values for the correction factor are stored in a lookup table, or the functional dependency of the correction factor from at least one property of the fluid is stored.
- 6. (Currently amended) Method according to [[one of the previous claims,]] claim

  1, wherein the balance flow (f<sub>bal</sub>) is order to achieve a temporary reduction of the external work flow (f<sub>ew</sub>) further down the working path is adjusted to a preset value that is high in comparison to the offset value.
- 7. (Currently amended) Method according to [[one of the previous claims,]] claim 1, wherein the resistance value if the adjustable fluidic resistance device for the determination of the internal work flow (f<sub>iw</sub>) and/oder and/or external work flow (f<sub>ew</sub>) further down the working path is temporarily set in such manner that a balance flow (f<sub>bal</sub>) [[(fbai)]] of unequal to zero results, and the internal work flow (f<sub>iw</sub>) [[(fiw)]] expected in normal operating mode and/or the external work flow (f<sub>ew</sub>) is determined from the signal (S<sub>vai</sub>) [[(Sbai)]] of the flow sensor (108).
- 8. (Original) Method according to claim 7, wherein the adjustable fluidic resistance device (110) is shorted for measuring the internal work flow ( $f_{iw}$ ) in the cross-

branch and/or adjusted to a value equal to zero, whereby the cross-branch preferably exhibits a fluidic resistance of equal to or near zero.

- 9. (Currently amended) Method [[Device]] for the supply of a defined fluid flow, [[in particular for liquid chromatography,]]
  - a) with a fluidic junction (5) splitting a total flow ( $f_0$ ) into an internal excess flow ( $f_{ie}$ ) inside an excess branch and an internal work flow ( $f_{iw}$ ) inside a working branch,
  - b) whereby the split ratio of the internal work flow (f<sub>iw</sub>) and the internal excess flow (f<sub>ie</sub>) is determined by the reverse ratio between a fluidic resistor (7) in the working branch and a fluidic resistor (9) in the excess branch, [[-]]
  - c) whereby the excess branch and the working branch are interconnected at the outputs of the two fluidic resistors (7, 9) by a cross-branch, and
  - d) whereby further down the working branch an external work flow (f<sub>ew</sub>) may be supplied to a working device, a chromatography column, for example,]] which may be connected to the device (100),
  - e) with a flow sensor (108) between the outputs of the fluidic resistors (7, 9) in the cross-branch to measure the balance flow  $(f_{bal})$ ,
  - f) whose sensor signal (S<sub>bal</sub>) is fed into a controller (112),
  - g) with a controllable, adjustable fluidic resistance device (110) further down the excess branch, controllable by a control device (112),
  - h) whereby the controller (112) adjusts the balance flow (f<sub>bal</sub>) by controlling the resistance value of the adjustable fluidic resistance device (110) in such manner that the balance flow (f<sub>bal</sub>) [[, preferably im zeitlichen Mittel,]] is zero or equal to a preset offset value, which is small in comparison to the internal work flow (f<sub>iw</sub>).

- 11. (Currently amended) Method according to claim 9, [[or 10,]] wherein the fluidic resistors (7, 9) are designed in such fashion that their fluidic throughput time is small in comparison to the duration of common solvent gradients.
- 12. (Currently amended) Method according to claim 9, [[to-11,]] wherein the fluidic resistances (7, 9) are configured in such fashion that they always exhibit the same temperature.
- 13. (Currently amended) Method according to claim 9, [[to 12,]] wherein the method according to claim 1 [[one the claims 1 to 8]] is executed by a controller (112).
- 14. (Currently amended) Method [[Device]] according to claim 1, [[one of the previous claims,]] wherein the total fluidic resistance value of the changeable fluidic resistance device (110) is composed of the resistance value of an adjustable, preferably electrically controlled fluidic resistance element (122) and a non-adjustable fluidic resistance element (120), wherein the fluidic resistance value [[, especially that of the non-adjustable fluidic resistance element (120)]] is dependent on the viscosity of the solvent being used.
- 15. (New) Method according to claim 1, wherein the operating device is a chromatography column.
- 16. (New) Method according to claim 3, wherein the at least one property of the fluid is the thermal conductivity or thermal capacity of the fluid.
- 17. (New) Method according to claim 4, wherein a correction factor is multiplied with the sensor signal (S<sub>bal</sub>).

## **PATENT**

- 18. (New) Method according to claim 9, wherein the working device is a chromatography column.
- 19. (New) Method according to claim 14, wherein the fluidic resistance value is that of the non-adjustable fluidic resistance element (120).